

Microfluidic Studies of CO₂ Sequestration by Frustrated Lewis Pairs

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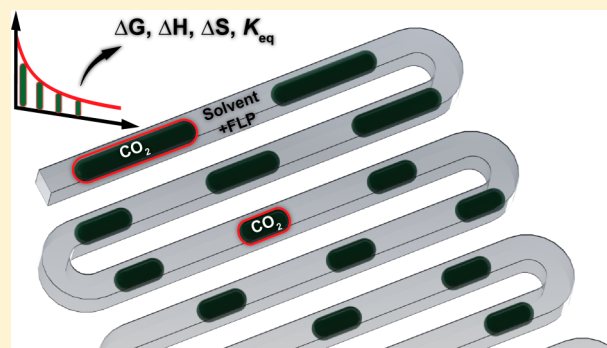
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S Supporting Information

ABSTRACT: Frustrated Lewis pairs (FLPs) comprising sterically hindered Lewis acids and bases offer the capability to reversibly capture CO₂ under mild reaction conditions. The determination of equilibrium constants and thermodynamic properties of these reactions should enable assessment of the efficiency of a particular FLP system for CO₂ sequestration and provide insights for design of new, efficient formulations of FLP catalysts for CO₂ capture. We have developed a microfluidic approach to studies of FLP–CO₂ reactions, which provides their thermodynamic characterization that is not accessible otherwise. The approach enables the determination of the equilibrium reaction constants at different temperatures, the enthalpy, the entropy, and the Gibbs energy of these reactions, as well as the enhancement factor. The microfluidic methodology has been validated by applying it to the well-characterized reaction of CO₂ with a secondary amine. The microfluidic approach can be applied for fundamental thermodynamic studies of other gas–liquid reactions.



INTRODUCTION

Elevated levels of carbon dioxide (CO₂) in the atmosphere are clearly influencing the progression of global warming. Strategies to manage atmospheric CO₂ concentrations include reducing emissions, sequestration and storage (e.g., in underground aquifers), or utilization of CO₂ as a C₁ chemical feedstock.^{1–3} The conversion of CO₂ to products such as formic acid and carbon monoxide⁴ or to readily usable fuels such as methanol^{5,6} remains a challenge due to the relatively low reactivity and high thermal stability of the CO₂ molecule. While a series of transition metal systems have been reported to effect reduction chemistry of CO₂,^{7–11} a unique alternative involves the use of frustrated Lewis pairs (FLPs).^{12–14} These systems, comprising sterically hindered Lewis acids and bases, act in concert to capture CO₂ under mild reaction conditions.¹⁵ Moreover, tuning the Lewis acidity and basicity of the FLPs alters their reactivity in reactions with CO₂ from reversible sequestration to stoichiometric and even catalytic reduction to methanol¹⁶ or CO.^{17–20}

Strategies to predict and design FLPs capable of the effective sequestration and activation of CO₂ necessitate a deeper understanding of the factors that influence the reaction. To this

end, the deliberate studies of the effects of FLP structure, concentrations, and reaction temperatures on the reactivity of FLP reagents are required. As the initial FLPs afforded reversible binding to CO₂, the determination of equilibrium constants and thermodynamic parameters of these reactions should enable assessment of the efficiency of a particular FLP system for CO₂ sequestration and provide predictive insights for design strategies targeting new and efficient formulations of FLP catalysts for CO₂ capture and reduction. Currently used batch-scale characterization methods^{21,22} for gas–liquid reactions involving CO₂ are time-consuming and plagued with an insufficient control over gas–liquid interfaces and diffusion control challenges associated with the large volumes of the reactors used. Measurements of a particular physical or chemical property require a relatively large quantity of reagents. Common spectroscopic characterizations of reaction products may be challenged by chemical exchange processes with the atmosphere. Moreover, when equilibrium constants of FLP–CO₂ reactions are high, the equilibrium thermodynamic

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characterization cannot be achieved using batch-scale methods.²³

Recently, the utilization of microfluidic (MF)-based platforms has been proposed to address some of these challenges by dramatically shrinking the dimensions of the reaction vessel from *centimeters* to *micrometers*, thereby reducing the diffusion length and time scales. Integration of in-line characterization tools with different MF devices has enabled high-throughput screening of the physical and chemical processes.^{24–30} In particular, a reduced mass transfer limitation and well-defined interfacial areas achieved in gas–liquid segmented flows have been utilized for chemical³¹ and physical^{32–35} screening of gas–liquid processes involving CO₂.

In the present paper, we report a MF strategy for fundamental thermodynamic studies of the reaction of CO₂ with FLP reagents. Using a MF approach, we calculated equilibrium constants of this reaction at different temperatures, assessed the thermal stability of the adduct, and determined the thermodynamic characteristics of the reaction, such as the enthalpy, entropy, and the Gibbs free energy. The proposed MF method can be used to acquire thermodynamic data for FLP–CO₂ reactions in 10–15 min and can be applied to fundamental studies of other reactions that include reactive gases.

EXPERIMENTAL SECTION

The reagents tri-*tert*-butylphosphine, *t*Bu₃P, and chlorobis(pentafluorophenyl)borane, ClB(C₆F₅)₂, were synthesized as described elsewhere²³ and dissolved in bromobenzene to various concentrations. Bromobenzene was purchased from Caledon (Canada) and distilled. The solutions of FLP reagents were prepared on the day of the MF experiments and stored in a glovebox (1.2–2 ppm O₂). The solutions of individual FLP reagents in bromobenzene were supplied to the MF reactor from two 1 mL gastight syringes (SGE Analytical Science), using the same syringe pump.

The configuration and dimensions of the MF reactor are shown in Figure S1, Supporting Information. Prior to MF experiments, the MF reactor was purged with dry CO₂ for 10 min at 2 psig to remove air. An inverted microscope (Olympus IX71) coupled to a CCD camera (Photometrics CoolSnap ES) was used for optical characterization of the CO₂ bubbles (plugs) and liquid segments (slugs). ImagePro (Media Cybernetics) software was used to acquire multiple sequences of bright-field images of the segmented flow on-chip. Analysis of the image sequence was carried out using a custom-developed MATLAB-based image processing code, which automatically measured the CO₂ plug length and plug position in a region of interest.^{34,35}

Physical dissolution of CO₂ in bromobenzene and in solutions of FLP reagents in bromobenzene was examined using attenuated total reflection Fourier transform infrared (ATR-FTIR) spectroscopy (Vertex 70, Bruker Corp.). Opus 6.5 software was used for spectral analysis.

The glass MF reactor was dried prior to each set of experiments to remove traces of water. Carbon dioxide gas was supplied from a gas tank at the pressure of 118.5 kPa using a digital servo pressure controller. The pressure drop along the microchannel was calculated based on the CO₂ plug velocity, void fraction, microchannel length, liquid viscosity, and the atmospheric pressure of 101.3 kPa at the outlet of the reactor (see Supporting Information, S2). The individual solutions of ClB(C₆F₅)₂ and *t*Bu₃P in bromobenzene with equal molar concentration were supplied to the MF reactor at a flow rate of 2.5 μL/min (the total volumetric flow rate of the mixed reagent solution was 5 μL/min). The total FLP concentration, C_{FLP}, in the mixed solution was changed from 0 to 50 mM. Experiments were performed at temperatures, *T*, of 273, 283, 293, 303, and 313 K.

RESULTS AND DISCUSSION

Figure 1a shows the chemical reaction of CO₂ with the FLP reagents, that is, ClB(C₆F₅)₂ and *t*Bu₃P, leading to the FLP–

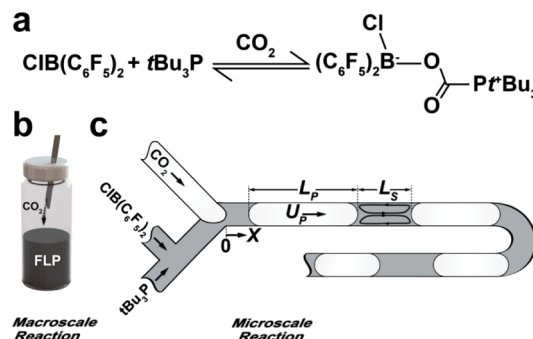


Figure 1. Reversible FLP–CO₂ reaction conducted in a MF reactor. (a) Reaction of FLP reagents, ClB(C₆F₅)₂ and *t*Bu₃P, with CO₂ in bromobenzene forming the FLP–CO₂ adduct. (b) Schematic of the batch-scale experiment. (c) Illustration of the CO₂ plugs and liquid slugs of FLP reagents with lengths *L_p* and *L_s*, respectively, forming at the Y-junction.

CO₂ adduct. Figure 1b illustrates the reaction conducted in a macroscopic format. The process involves bubbling CO₂ into the FLP solution at a fixed pressure, which is followed by the isolation, drying, and analysis of the precipitated product, ClB(C₆F₅)₂–CO₂–*t*Bu₃P. Generally, one experiment takes ~2 h from reaction to analysis. The isolated product may undergo a facile loss of CO₂, which is accelerated with increasing temperature. Figure 1c illustrates the same reaction conducted in the continuous mode in a MF reactor using alternating flow of CO₂ plugs and liquid reagent segments (slugs). In our work, the solution of FLP reagents in bromobenzene and the CO₂ gas were supplied via two inlets into the MF reactor. The ClB(C₆F₅)₂ and *t*Bu₃P reagents were mixed in-line, using a T-junction, before entering the MF device. The liquid reagents and CO₂ converged at the Y-junction, where the gas stream periodically broke up to produce gaseous CO₂ plugs separated by liquid reagent slugs. Following dissolution of CO₂ in an adjacent liquid slug, it reacted with the FLP reagents. As a result of these two processes, the gaseous CO₂ plugs shrank. Two recirculation zones inside each liquid segment enhanced mixing and mass transfer of CO₂ molecules into the liquid phase by convective transport (Figure 1c).

The total change in dimensions of the CO₂ plugs was determined by three factors: (i) the drop in pressure along the microchannel, (ii) the physical dissolution of CO₂ in bromobenzene, and (iii) the chemical reaction of CO₂ with FLP reagents (Supporting Information, Figure S2). The first effect led to the expansion of CO₂ plugs, while the other two effects led to gaseous plug shrinkage. At equilibrium, the physical dissolution and reaction-induced reduction in CO₂ plug dimensions were temporarily balanced by the pressure drop along the channel, and the size of the CO₂ plugs remained constant.

In the course of experiments, we monitored the variation in the length of CO₂ plugs, *L_p*, when CO₂ dissolved in the adjacent liquid segment with the length *L_s* (*L_s* remained approximately constant). By accounting for the expansion of the gas plug due to the pressure drop,³² we evaluated the amount of CO₂ transferred from the gas plugs to the liquid slugs. Since the initial size of the generated CO₂ plugs was

sufficiently large to retain their plug-like shape after CO₂ dissolution, we assumed that the gas plugs and the liquid slugs moved with the same velocity, and in this manner, we converted the distance traveled by the plugs and slugs into reaction time, t (see Supporting Information, S2).

Assuming an ideal gas behavior, we calculated the time-dependent volume of CO₂ plugs, V_p , and the number of moles of CO₂, $n_{\text{CO}_2}(t)$, in the plug at time t as

$$n_{\text{CO}_2}(t) = \frac{PV_p}{RT} \quad (1)$$

where P is the pressure in the plug after accounting for pressure drop at each location, R is the gas constant ($R = 8.314 \text{ J mol}^{-1} \text{ K}^{-1}$), and T is the temperature of the system. The total number of moles of CO₂ transferred from the plug equaled the number of CO₂ moles entering the liquid segment, and the concentration of CO₂ in the liquid was calculated as

$$C_{\text{tot}}(t) = \frac{n_{\text{CO}_2}(t=0) - n_{\text{CO}_2}(t)}{V_s} \quad (2)$$

where $C_{\text{tot}}(t)$ is the total concentration of CO₂ in the liquid slug at time t ; $n_{\text{CO}_2}(t=0)$ and $n_{\text{CO}_2}(t)$ correspond to the number of moles of CO₂ in the plug at time $t=0$ and t , respectively, and V_s is the volume of the adjacent liquid slug.

Prior to MF experiments, we ensured that physical dissolution of CO₂ in the liquid medium does not change in the presence of FLP reagents. We conducted attenuated total reflection Fourier transform infrared spectroscopy characterization of the physical dissolution of CO₂ in reagent-free bromobenzene, as well as in bromobenzene solutions containing 80 mM *t*Bu₃P, 80 mM ClB(C₆F₅)₂, and 160 mM of the FLP reagents (Figure 2a). We monitored the intensity of

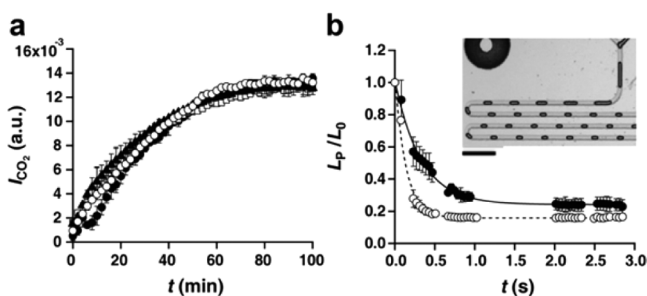


Figure 2. (a) Variation in intensity of the IR band at 2343 cm^{-1} associated with physically dissolved CO₂ in bromobenzene (\blacktriangle), in a solution of 80 mM *t*Bu₃P (\square) or 80 mM ClB(C₆F₅)₂ (\circ) in bromobenzene, and in an equimolar solution of 160 mM *t*Bu₃P and ClB(C₆F₅)₂ in bromobenzene (\bullet). (b) Variation in the normalized length of the CO₂ plug with time for the CO₂–bromobenzene (\bullet) and CO₂–FLP solution in bromobenzene at the total FLP concentration of 40 mM FLP (\circ); $T = 293 \text{ K}$. Each experimental point is the average of three results obtained under identical conditions. The inset shows an optical microscopy image of segmented flow with CO₂ plugs (dark color) and slugs of FLP solution in bromobenzene (light color). The scale bar is $500 \mu\text{m}$.

the IR peak corresponding to physically dissolved CO₂, I_{CO_2} , at 2343 cm^{-1} . The equilibrium intensity of the peak was reached after 80 min, with identical peak intensity for all the four solutions tested. This result indicated that the physical uptake of CO₂ by bromobenzene was not affected by the presence of individual FLP reagents or a 1:1 mixture of the reagents. On the

basis of these results, we used the dissolution of CO₂ in bromobenzene as a reference system for the MF studies of the FLP–CO₂ reaction. We note that the time scale difference between the ATR-FTIR and MF experiments (90 min and 1 s in Figure 2a,b, respectively, needed for liquid saturation with CO₂) is associated with the CO₂ diffusion length difference for these experiments. Similar time scales for both experiments can be achieved if the ATR-FTIR characterization was performed on the same length scale as the MF experiments (Supporting Information, S3).

Figure 2b shows the representative variation in the normalized length, L_p/L_0 , of the CO₂ plugs in bromobenzene and an FLP solution, where L_0 is the initial CO₂ plug length formed after the Y-junction. Figure 2, inset, illustrates the shrinkage of CO₂ plugs. Under similar pressure and temperature, the ratio L_p/L_0 was significantly smaller for the system containing FLP reagents than for the FLP-free system, as a result of FLP reaction with CO₂.

Using eqs 1 and 2, we converted the change in volume of the CO₂ plugs into C_{tot} for different FLP concentrations (Figure 3a). With increasing reaction time, t , the concentration of CO₂

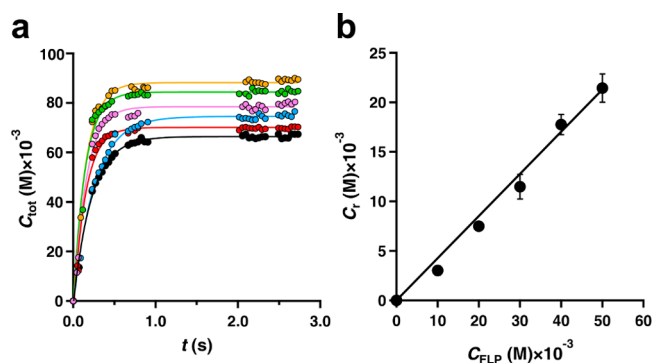


Figure 3. (a) Variation in total molar concentration of CO₂ transferred at 273 K from the gas phase (plugs) to the solution with FLP concentration of 0 mM (black), 10 mM (red), 20 mM (blue), 30 mM (pink), 40 mM (green), and 50 mM (orange). The gaps in the data points appear due to the MF reactor geometry (Supporting Information, Figure S1). (b) Variation in the equilibrium concentration of chemically reacted CO₂, plotted as a function of the initial FLP concentration at $T = 273 \text{ K}$. Each experimental point is the average of three experiments conducted under identical conditions. Three hundred images were acquired for each experiment with at least 4000 CO₂ plugs.

in the liquid slugs increased, and the equilibrium was reached after $\sim 2 \text{ s}$. The equilibrium CO₂ uptake by the liquid slugs increased with increasing concentrations of *t*Bu₃P and ClB(C₆F₅)₂, indicating that the FLP reagents were the limiting reagents. The CO₂ uptake caused by the chemical reaction, C_r , was determined by subtracting the equilibrium C_{tot} (for the CO₂–bromobenzene system) from the total equilibrium uptake of CO₂, C_{tot} , for the FLP–CO₂ system. Figure 3b shows that the value of C_r increased linearly with FLP concentration.

Since the reaction between ClB(C₆F₅)₂, *t*Bu₃P, and CO₂ is exothermic, local heat accumulation immediately downstream of the Y-junction could be expected if the rate of heat generation was faster than heat distribution and dissipation through the walls of the MF reactor. Such accumulation could affect the reaction kinetics and the gas plug size over the course of the reaction but would not affect the thermodynamics of the reaction (see Supporting Information, Figure S4). The

invariance of CO₂ plug volume after the equilibrium point (Figure 3a) indicated that the heat generated during the CO₂–FLP reaction has been dissipated before the reaction reached the equilibrium.

Following the approach established for the CO₂–FLP reaction at 273 K, we studied the equilibrium chemical uptake of CO₂ by the FLP reagents at 283, 293, 303, and 313 K. The entire MF reactor and a section of the tubings supplying the gaseous CO₂ and the liquid reagents to the MF reactor were immersed in a water bath maintained at the desired temperature. The submersion of the tubing was especially important for the CO₂ gas in order to avoid temperature-mediated, rather than reaction-induced, changes in the CO₂ plug volume. Figure 4 shows that the value of C_r varied linearly with the FLP concentration in the entire temperature range studied.

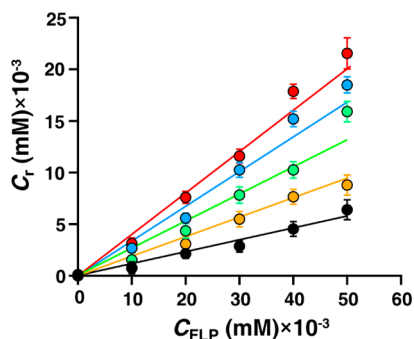


Figure 4. Variation in the equilibrium reaction-induced chemical CO₂ uptake, plotted as a function of the initial concentration of FLP reagents in the adjacent liquid slugs for 273 K (red), 283 K (blue), 293 K (green), 303 K (orange) and 313 K (black).

For similar concentrations of FLP reagents, the value of C_r reduced with increasing temperature. This trend resulted from the reverse FLP–CO₂ reaction, which was favored at elevated temperatures¹⁰ and led to the release of CO₂ from the adduct. As a result, the highest conversion of FLP reagents was achieved at 273 K. Using the data plotted in Figure 4, the equilibrium constant, K_{eq}, of the FLP–CO₂ reaction at a particular temperature was determined as

$$K_{\text{eq}} = \frac{[\text{CIB}(\text{C}_6\text{F}_5)_2 - \text{CO}_2 - t\text{Bu}_3\text{P}]}{[\text{CIB}(\text{C}_6\text{F}_5)_2][t\text{Bu}_3\text{P}]C_{\text{tot}}(\text{bromobenzene})} \quad (3)$$

where [CIB(C₆F₅)₂–CO₂–tBu₃P] is the concentration of the FLP–CO₂ adduct, equal to C_r (determined from Figure 3b), [CIB(C₆F₅)₂] and [tBu₃P] are the equilibrium concentrations of the reagents, calculated as C_r – [CIB(C₆F₅)₂]_{initial} and C_r – [tBu₃P]_{initial}, respectively, and C_{tot}(bromobenzene) is the equilibrium concentration of CO₂ dissolved in bromobenzene (Figure 3a). For the calculation of K_{eq}, the reaction of CO₂ with CIB(C₆F₅)₂ and tBu₃P was assumed to be stoichiometric and side reactions were ignored. Upon the reaction with FLP reagents, CO₂ is replenished by the continuous dissolution of CO₂ from gaseous plugs, thus maintaining the total supply of CO₂ in the solution. Using eq 3, the equilibrium constants for the FLP–CO₂ reaction carried out at 273, 283, 293, 303, and 313 K were calculated to be 687, 431, 223, 141, and 75 M^{–2}, respectively.

Next, we calculated the Gibbs free energy of the reaction, ΔG, at 273, 283, 293, 303, and 313 K as

$$\Delta G = -RT \ln(K_{\text{eq}}) \quad (4)$$

and obtained the values of ΔG to be –14.8, –14.3, –13.2, –12.5, and –11.2 kJ mol^{–1}, respectively.

We then determined the enthalpy and the entropy of the FLP–CO₂ reaction, ΔH and ΔS, by using the van't Hoff equation³⁶

$$\ln(K_{\text{eq}}) = -\frac{\Delta H^0}{RT} + \frac{\Delta S^0}{R} \quad (5)$$

and plotting ln(K_{eq}) versus 1/T, a graph with the slope of –ΔH/R and the y-intercept of ΔS/R (Figure 5).

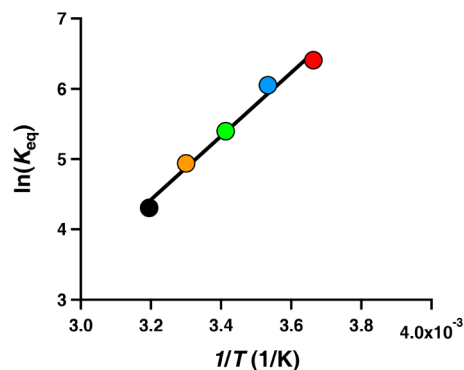


Figure 5. Variation of ln(K_{eq}) with reaction temperature. Based on eq 5, the slope of the graph yields –ΔH/R.

A linear dependence of ln(K_{eq}) versus 1/T indicated that ΔH does not appreciably change with temperature over the range studied. The best fit of the linear dependence ln(K_{eq}) versus 1/T yielded a ΔH value of –39.3 kJ mol^{–1}. We independently estimated ΔS as –(ΔG – ΔH)/T and obtained the values of –89.3, –88.1, –88.8, –88.2, and 89.3 J mol^{–1} K^{–1}, for the temperatures 273, 283, 293, 303, and 313 K, respectively. Table 1 shows the summary of thermodynamic characteristics of the FLP–CO₂ reaction.

Table 1. Thermodynamic Characteristics of the FLP–CO₂ Reaction

T (K)	273	283	293	303	313
K _{eq} (M ^{–2})	687	431	223	141	75
ΔH ^a (kJ mol ^{–1})	–39.3	–39.3	–39.3	–39.3	–39.3
ΔS (J mol ^{–1} K ^{–1})	–89.3	–88.1	–88.8	–88.2	–89.3
ΔG (kJ mol ^{–1})	–14.8	–14.3	–13.2	–12.5	–11.2

^aThe value of ΔH is determined from the slope of the graph in Figure 5.

Finally, we calculated the enhancement factor, E, which describes the influence of a reaction on mass transfer and is defined as the ratio of total absorption of gas by a reactive liquid to the physical absorption of the gas under identical conditions.^{37,38} The positive deviation of E from unity reflects the effect of a chemical reaction on increased uptake of a gas by the liquid medium.³⁹ We determined the value of E as the number of moles of CO₂, Δn_{CO₂,chem-phys}, transferred into the FLP solution divided by the number of moles of CO₂, Δn_{CO₂,phys}, transferred in bromobenzene as

$$E = \left(\frac{\Delta n_{\text{CO}_2, \text{chem-phys}}}{\Delta n_{\text{CO}_2, \text{phys}}} \right) \quad (6)$$

The enhancement factor was determined for different FLP concentrations and different temperatures and is summarized in Table 2. As expected, the value of E increased with an increase in FLP reagent concentration and with decreasing temperature.

Table 2. Enhancement Factor of the FLP–CO₂ Reaction

	[FLP] (mM)					
	10	20	30	40	50	
	273	1.05	1.12	1.18	1.27	1.33
	283	1.04	1.08	1.16	1.23	1.28
T (K)	293	1.02	1.06	1.11	1.15	1.23
	303	1.01	1.06	1.10	1.14	1.16
	313	1.01	1.03	1.04	1.07	1.09

We validated the MF methodology by applying it to the well-characterized reaction between CO₂ and diethanolamine and comparing the experimentally obtained enthalpy with the reported literature values. The value of ΔH of -69 kJ mol^{-1} obtained in the MF CO₂–diethanolamine experiments compared favorably with the values of ΔH in the range of $-71 \pm 4 \text{ kJ mol}^{-1}$, obtained by calorimetry, NMR, and solubility methods (Table S1, Supporting Information).

CONCLUSIONS

In summary, we developed a time- and labor-efficient MF platform for real-time, high-throughput studies of thermodynamics of FLP–CO₂ reactions. The approach presented here was validated for the reaction between CO₂ and diethanolamine. The equilibrium constants, Gibbs energy, enthalpy, and entropy of the FLP–CO₂ reaction were determined at different temperatures. In addition, we determined the enhancement factor under different reaction conditions. The proposed MF strategy provides access to the thermodynamic characterization of FLP–CO₂ reactions that is not accessible otherwise and can be applied to other gas–liquid reactions.

ASSOCIATED CONTENT

Supporting Information

Microfluidic experimental setup, methods of data acquisition and analysis, and infrared spectroscopy experiments. This material is available free of charge via the Internet at <http://pubs.acs.org>.

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Notes

The authors declare no competing financial interest.

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